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Citation: Applied Physics Letters 104, 131108 (2014); doi: 10.1063/1.4869561 View online: http://dx.doi.org/10.1063/1.4869561 View Table of Contents: http://scitation.aip.org/content/aip/journal/apl/104/13?ver=pdfcov Published by the AIP Publishing

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Design for high-power, single-lobe, grating-surface-emitting quantum cascade lasers enabled by plasmon-enhanced absorption of antisymmetric modes

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(Received 1 January 2014; accepted 12 March 2014; published online 3 April 2014)

Resonant coupling of the transverse-magnetic polarized (guided) optical mode of a quantum-cascade laser (QCL) to the antisymmetric surface-plasmon modes of 2nd-order distributed-feedback (DFB) metal/semiconductor gratings results in strong antisymmetric-mode absorption. In turn, lasing in the symmetric mode, that is, surface emission in a single-lobe far-field beam pattern, is strongly favored over controllable ranges in grating duty cycle and tooth height. By using core-region characteristics of a published 4.6 μ m-emitting QCL, grating-coupled surface-emitting (SE) QCLs are analyzed and optimized for highly efficient single-lobe operation. For infinite-length devices, it is found that when the antisymmetric mode is resonantly absorbed, the symmetric mode has negligible absorption loss $(\sim 0.1 \text{ cm}^{-1})$ while still being efficiently outcoupled, through the substrate, by the DFB grating. For finite-length devices, 2nd-order distributed Bragg reflector (DBR) gratings are used on both sides of the DFB grating to prevent uncontrolled reflections from cleaved facets. Equations for the threshold-current density and the differential quantum efficiency of SE DFB/DBR QCLs are derived. For 7 mm-long, 8.0 μ m-wide, 4.6 μ m-emitting devices, with an Ag/InP grating of ~39% duty cycle, and $\sim 0.22 \,\mu\text{m}$ tooth height, threshold currents as low as 0.45 A are projected. Based on experimentally obtained internal efficiency values from high-performance QCLs, slope efficiencies as high as 3.4 W/A are projected; thus, offering a solution for watt-range, single-lobe CW operation from SE, mid-infrared QCLs. © 2014 AIP Publishing LLC. [http://dx.doi.org/10.1063/1.4869561]

Grating-coupled surface-emitting lasers (GCSEL) are attractive sources due to easy packaging, lack of emittingfacet heating and subsequent degradation, ability to reach 1 W diffraction-limited continuous-wave (CW) power,¹ and the potential for obtaining multi-watt CW diffraction-limited power when combined with single-lateral-mode, high-indexcontrast photonic-crystal structures.²

Research on GCSELs started in the early 1970s and was focused on near-infrared (IR)-emitting devices.^{3–6} It was found for TE-polarized lasers that, in accordance with theory,⁷ the longitudinal mode favored to lase is the antisymmetric one (i.e., a mode whose far-field pattern consists of two lobes) due to its inherent low radiation loss and subsequent low threshold gain. Several approaches have been proposed and demonstrated for realizing operation in a singlelobe beam⁸ with the most successful ones being those involving no penalty in efficiency: central grating π phase shift^{9–11} or chirped grating corresponding to a π phase shift.¹

With the advent of quantum cascade lasers (QCLs) in the mid 1990s, GCSEL analysis turned to devices generating transverse-magnetic (TM)-polarized light.¹² SE distributed-feedback (DFB) grating, mid-IR-emitting QCLs include: two-dimensional (2-D) photonic-crystal structures,¹³ air-metal/semiconductor gratings,¹⁴ metal/semiconductor gratings for emission only through the substrate,^{15,16} metal/semiconductor biperiodic gratings,¹⁷ and all-semiconductor gratings.^{18,19} By

and large, the antisymmetric mode was found to be favored to lase, just like for TE-polarized GCSELs, with two exceptions: (a) excitation of a 2nd-order DFB region from a 1st-order DFB laser¹⁶ which gave a single, diffraction-limited beam only for short ($\leq 200 \,\mu$ m) apertures and (b) an edge- and surface-emitting device¹⁹ that provided 100 mW CW surfaceemitted power in a near-diffraction-limited beam, with significant power being edge emitted, and occasional two-lobed beams due to uncontrolled facet reflections. 500 mW CW surface-emitted power was reported from ring-cavity devices,¹⁸ but operating multimode. More recently,²⁰ ring-cavity GCSE QCLs have provided a symmetric-like, multilobe beam pattern, as a result of employing two π phase shifts and a linear-polarization scheme. THz SE-DFB QCLs have been found to operate in the antisymmetric mode as well with the solution for single-lobe operation being either a central π phase shift^{21,22} or symmetric-mode selection via dual-slit unitcell gratings²³ or gratings chirped from their centers to their edges.²⁴ Furthermore, by using resonant leaky-wave coupling,25,26 2-D GCSE THz QCLs emitting in diffractionlimited beams have been demonstrated.^{27,28}

Here, we present a GCSE QCL mid-IR-emitting structure with inherent suppression of the antisymmetric modes that allows symmetric-mode lasing at low (<0.5 A) threshold currents and high (>3 W/A) slope efficiencies. The device relies on the antisymmetric modes being strongly absorbed due to resonant coupling of the (guided) optical mode to the antisymmetric surface plasmon mode of a metal/semiconductor grating. In addition, the DFB grating is bounded by 2nd-order

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distributed Bragg reflector (DBR) gratings;^{1,8–10} thus, preventing uncontrolled reflections from cleaved facets, which can affect the DFB operation,¹⁹ as well as catastrophic facet degradation at high powers due the thermally induced sheer stress.²⁹ By considering a 4.6 μ m-emitting QCL structure which was previously reported to edge-emit watt-range CW power,³⁰ we find that 7.03 mm-long DFB/DBR GCSE devices can have threshold currents as low as 0.45 A and slope efficiencies as high as 3.4 W/A; thus, making it possible to obtain watts of CW diffraction-limited, single-lobe power from mid-IR surface-emitting QCLs. First, we analyze devices of infinite-length metal/semiconductor 2nd-order DFB gratings, in order to elucidate the mechanism via which the antisymmetric mode is suppressed. Then, we present the design and analysis of 2nd-order DFB/DBR devices of finite-length gratings, and provide examples of high-performance devices.

The antisymmetric surface plasmon mode at the interface(s) of a 2nd-order metal/semiconductor has its H-field intensity nulls occur in the middle of the grating troughs and peaks [see example in Fig. 1(b)]. For an infinite-length grating with Ag for metal, InP for semiconductor and designed to be the 2nd-order DFB grating for a published³⁰ 4.6 μ memitting QCL structure, we plot in Fig. 1(a) the wavevector of the plasmon as a function of grating duty cycle, defined as the percentage of metal in a grating period, and grating tooth height. A thin white line indicates the plasmon-wavevector curve corresponding to 4.6 μ m wavelength, λ ; that is, where the DFB-QCL structure's optical-mode propagation constant matches the plasmonmode propagation constant, and thus resonant coupling occurs between the two modes. We show in Fig. 1(b)



FIG. 1. Infinite-length grating: (a) Plasmon wavevector as function of grating duty cycle and tooth height for Ag/InP grating designed to be 2nd-order DFB grating for a published 4.6 μ m-emitting QCL.³⁰ The white line corresponds to resonant coupling between the (guided) optical mode and the anti-symmetric plasmon mode; (b) H-field intensity pattern at a resonance point: 39% duty cycle and 0.217 μ m grating tooth height, at $\lambda = 4.6 \,\mu$ m.

the plasmon H-field intensity for a grating of 39% duty cycle and 0.217 μ m tooth height ($\lambda = 4.6 \mu$ m).

Next, we consider the DFB-QCL structure for which the (transverse) optical mode couples to the grating surfaceplasmon modes. Coupling to the antisymmetric and symmetric plasmon modes results in antisymmetric (A) and symmetric (S) longitudinal modes of the structure. We choose a 40-period, 4.6 μ m-emitting QCL structure³⁰ of 75% transverse optical-confinement factor Γ . The grating period Λ is fixed to be that ratio of the vacuum wavelength (4.6 μ m) to the effective refractive index of the transverse mode, such that the 2nd-order Bragg-diffraction condition is met. For this 2nd-order DFB-QCL structure, we show in Fig. 2 the dispersion curves, at 39% grating duty cycle, for the A and S modes as a function of tooth height, h. As seen from the inserted pictures, in the case of the A mode for $h < 0.217 \,\mu\text{m}$ the guided mode couples in-phase with the antisymmetric plasmon mode, while for $h > 0.217 \,\mu\text{m}$ the guided mode couples outof-phase with the antisymmetric plasmon mode. The S mode couples weakly to the symmetric plasmon mode, as evidenced by negligible field at the grating interfaces. (However, the S-mode couples strongly to the grating and is effectively outcoupled over a large range in h [Fig. 3(b)].) Such modal behavior is somewhat similar to that for the modes of 1st-order metal/semiconductor DFB structures,³¹ in that the A and S modes qualitatively behave like the 1st-order DFB modes whose H-field maxima occur on the grating troughs and peaks, respectively (Fig. 3 in Ref. 31).

Fig. 3(a) shows the A-mode loss as a function of grating height and duty cycle. We superimpose the white line from Fig. 1(a) on the locus of maximum-loss points, to highlight that the latter corresponds to resonant coupling between guided and plasmon modes. The losses for the A and S modes are shown in Fig. 3(b) as the grating height varies, when the duty cycle is 39%. The A-mode loss is only absorption loss which is peaked at resonance (i.e., at $h = 0.217 \,\mu$ m). The S mode has both surface-emission (coupling coefficient $\kappa = 0.193 - i9.231 \,\text{cm}^{-1}$) and absorption losses; the latter being negligible (~0.1 cm⁻¹) due to weak optical-mode coupling to the symmetric plasmon mode. We note that significantly enhanced absorption of incident TM-polarized light, due to strong coupling to a surface-plasmon mode of a



FIG. 2. Normalized frequencies for the symmetric (S) and antisymmetric (A) modes of 4.6 μ m-emitting 2nd-order DFB-QCL structure, at 39% grating duty cycle, as a function of grating tooth height, *h*. Insets: H-field amplitude patterns. The A-mode is shown below and above resonance at *h* = 0.217 μ m.

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FIG. 3. (a) The antisymmetric (A)-mode loss as a function of grating duty cycle and tooth height. The white line atop the locus of maximum-loss points is the same white line as in Fig. 1(a), confirming that the A-mode maximum loss occurs at grating parameters corresponding to resonant coupling between guided and plasmon modes. (b) Intensity loss coefficient⁸ for the symmetric and antisymmetric modes as a function of grating height when the grating duty cycle is 39%. The S-mode absorption loss is negligible.

2nd-order DFB metal grating, has previously been obtained³² for proposed high-performance mid-IR photodetectors.

Next, we study finite-length, buried-heterostructure devices with DBR gratings at the ends of the DFB grating (Fig. 4), just as for high-power, near-IR GCSELs.^{1,8–10} A longitudinal cross-section is shown in the inset. The 40-period InGaAs/InAlAs core region of a high-CW-power, $4.6 \,\mu$ m-emitting QCL³⁰ is considered. Atop an InP cladding layer a metal/semiconductor grating is placed. To control the tooth height, a 10 nm-thick InGaAs etch-stop layer [Fig. 1(b)] is introduced between the InP cladding layer and the grating. At the top of the semiconductor portions of the grating, a 50 nm-thick n⁺-InP layer is added [Fig. 1(b)] to ensure good electrical contact, and 2 nm-thick Ti layers are inserted between metal and semiconductor for good adhesion.

For finite-length devices, the coupled-mode theory for 2nd-order metal/semiconductor gratings is employed⁷ together with the matrix method for DFB/DBR structures⁸ adjusted for TM-polarized light. More specifically, COMSOL is used to calculate the eigenfrequencies of the symmetric and antisymmetric modes for an infinite-length DFB structure.⁷ The real and imaginary parts of these are converted into detuning and loss parameters, both in units of



FIG. 4. Schematic representation of surface-emitting, buried-heterostructure DFB/DBR QCL for operation at 4.6 μ m wavelength.

cm⁻¹, and then inserted into the equations for calculating the coupling coefficient and correction factor.⁷ Then, we use the transfer-matrix method to solve for the grating-related (intensity) loss coefficient,⁸ 2α , which is part of the *local* threshold gain (i.e., in the DFB region) g_{th},^{2,8} which, for interband-transition devices, is given by

$$g_{th} = 2\alpha + \frac{\alpha_i}{\Gamma_{lg}},\tag{1}$$

where α_i is the internal cavity loss and Γ_{lg} is the percentage of field intensity residing in the DFB region. However, for QCLs one has to take into account the backfilling-current density³³ and the leakage-current density³³ which, multiplied by Γg , are routinely subsumed with α_i as being parts of a "waveguide" loss coefficient α_w in the threshold-current density formula for Fabry-Perot-cavity devices: $J_{th} = (\alpha_m + \alpha_w)/\Gamma g$, where α_m is the mirror loss and g is the differential gain. Since backfilling and carrier leakage occur only in the DFB region, the g_{th} equation for SE DFB/DBR QCLs is

$$g_{th,q} = 2\alpha + \alpha_w + \left(\frac{1}{\Gamma_{lg}} - 1\right)\alpha_i.$$
 (2)

For α_w we take the experimental value obtained³⁰ by Lyakh *et al.*: 3.3 cm⁻¹, and for α_i we take a value of 0.5 cm⁻¹, typical of state-of-the-art, high-power 4.5–5.0 μ m-emitting QCLs.^{34,35} The modal threshold gain² $G_{th,q} = \Gamma_{lg}g_{th,q}$. Then, the threshold-current density is

$$J_{th} = \frac{G_{th,q}}{\Gamma_{lg}\Gamma g} = \frac{g_{th,q}}{\Gamma g}.$$
(3)

The finite-length structure chosen for analysis is one that maximizes the outcoupling loss for the S mode, while maintaining a low value (i.e., 2) for the S-mode guided-field-intensity peak-to-valley ratio in the DFB region⁸ R_0 ; chosen to prevent multimoding at high-drive levels due to longitudinal gain spatial hole burning. Then, for a 7.03 mm-long device of 3.07 mm-long DFB region and 1.98 mm-long DBR regions, we find for the S mode that $2\alpha = 5.98 \text{ cm}^{-1}$ and $\Gamma_{\text{lg}} = 0.81$. In turn, $g_{\text{th},q}$ has a value of 9.4 cm^{-1} and the G_{th} value is 7.6 cm⁻¹. Fig. 5(a) shows the $g_{\text{th},q}$ values for A and S modes, as a function of detuning from the reference $4.6 \,\mu\text{m}$ wavelength, for a grating of 39% duty cycle and 0.217 μ m height.

An S mode is clearly favored to lase over two adjacent A modes, which have $g_{th,q}$ values 23.1 cm^{-1} and 23.9 cm^{-1} higher than the S mode. These large intermodal-discrimination values are dominated by the strong absorption of the A modes. For the S mode, by using Eq. (3) and the *g* value experimentally obtained by Lyakh *et al.*,³⁰ we obtain a J_{th} value of 1.84 kA/cm^2 . Then, for a 3.07 mm-long DFB region and a 8.0 μ m-wide buried-ridge guide,³⁶ as needed for operation primarily in the fundamental lateral mode,³⁷ the threshold current is 0.45 A, a value comparable to those of state-of-the-art, high-power edge-emitting QCLs operating in the 4.5–5.0 μ m range.^{34,35}



FIG. 5. (a) Local threshold gain $g_{th,q}$ for S and A modes, at 39% duty cycle and 0.217 μ m grating height, as a function of detuning from the 4.6 μ m reference wavelength. (b) $g_{th,q}$ for S and A modes vs. grating height, at 39% duty cycle. (c) Intermodal discrimination vs. grating height and duty cycle.

Fig. 5(b) shows the $g_{th,q}$ values for the S and the two adjacent A modes as a function of grating height, at 39% duty cycle. The A modes reach gth.q maxima at values corresponding to resonant coupling of the guided mode to the antisymmetric plasmon mode, at their respective oscillation wavelength. The intermodal discrimination is $\geq 10 \text{ cm}^{-1}$ over a $0.030 \,\mu\text{m}$ -wide variation in tooth height, which is quite achievable by using a stop-etch layer. Fig. 5(c) shows the intermodal discrimination as a function of duty cycle and tooth height. Thin black lines indicate where the intermodal discrimination is 10 cm⁻¹; thus, defining a curved-stripeshaped domain over which the intermodal discrimination is $\geq 10 \,\mathrm{cm}^{-1}$. For a fixed duty cycle, intermodal discrimination is $\geq 10 \text{ cm}^{-1}$ over a 0.030 μ m-wide variation in tooth height (e.g., over the 0.202–0.232 μ m range in tooth height at 39% duty cycle). This can easily be achieved by using the InGaAs stop-etch layer. For a fixed tooth height, intermodal discrimination is $\geq 10 \text{ cm}^{-1}$ over a 2%-wide variation in duty cycle (e.g., over the 38%–40% range in duty cycle at 0.217 μ m tooth height). For a grating of $1.44 \,\mu m$ period, this corresponds to controlling the tooth width within 0.03 μ m, which can be achieved with e-beam lithography.

A study over the ranges: 37%-41% in duty cycle and $0.202-0.232 \,\mu\text{m}$ in grating height, within the $\geq 10 \,\text{cm}^{-1}$ domain, reveals that the grating outcoupling efficiency decreases by at most 15% (i.e., from 40% to 34%). 40% outcoupling efficiency is obtained for 38%, 39% and 40% duty cycle at 0.202 μ m, 0.217 μ m and 0.232 μ m grating height, respectively. Thus, the chance of getting outcoupling efficiencies close to 40% is high. Finally, if the grating height is controlled, via the etch-stop layer, to be within the 0.03 μ m range, the range of acceptable duty-cycle values is 4%: from 37% to 41%; thus, the actual tolerance in grating-tooth width is 0.06 μ m, which can be controlled via e-beam lithography.

Figs. 6(a) and 6(b) show the *radiated* near-field intensity^{8,9} and the envelope of the guided-field intensity profiles for S and A modes, when the grating duty cycle and tooth height are 39% and 0.217 μ m. The R_0 value is only 2, as required to ensure single-longitudinal-mode operation to high drive levels.^{1,8} For the A modes the guided-field intensity in



FIG. 6. Near-field intensity and envelope of guided-field intensity profiles for (a) S and (b) A modes, at 39% duty cycle and 0.217 μ m grating height. (c) Far-field beam pattern for the S mode.

the DFB region is fairly uniform, yet peaks in the center of the DFB region. Considering this, the fact that the intermodal discrimination is $>20 \text{ cm}^{-1}$ and that $R_0 = 2$, it is quite reasonable to assume that longitudinal spatial hole burning is unlikely to cause multimoding at high drives above threshold. Fig. 6(c) is the S-mode far-field beam pattern: a single lobe.

As for the differential quantum efficiency, the equation for GCSELs^{2,8} modified for QCLs is

$$\eta_d = \eta_i \ \frac{\alpha_{surf}}{G_{th}} N_p = \eta_p \eta_{tr} \frac{\alpha_{surf}}{2\alpha \Gamma_{lg} + \alpha_i} N_p, \tag{4}$$

where α_{surf} is the surface radiation loss;² η_i is the internal differential efficiency per period,³⁸ the product of η_p , the differential pumping efficiency, and η_{tr} , the transition differential efficiency; and N_p is the period number. The α_{surf}/G_{th} term, known as outcoupling efficiency, is 40% in this case. While for devices with suppressed carrier leakage (i.e., $\eta_{\rm p}$ close to unity) the η_i value is theoretically ~0.85, the best reported^{35,39} experimental values are in the 0.70-0.79 range. Then, taking $N_{\rm p} = 40, \, \lambda = 4.6 \, \mu {\rm m}$, and assuming an AR-coated window and negligible substrate absorption, the estimated slope efficiencies are 3.0-3.4 W/A, values comparable to best reported pulsed, single-facet values from 4.6 µm-emitting devices. Furthermore, for devices with $R_0 = 2.5$ the outcoupling efficiency increases to 48%; then, the slope efficiencies are in the 3.6-4.1 W/A range. Since gain spatial hole burning is not well understood in QCLs, we chose to analyze the more conservative case of $R_0 = 2$, but that does not mean that devices of $R_0 = 2.5$ are not possible candidates for single-mode operation to watt-range powers.

Using the estimated threshold and slope-efficiency values (i.e., 0.45 A and 3.4 W/A), the projected peak pulsed power at $3 \times$ threshold is 3.06 W. The coherent power can be increased via resonant leaky-wave coupling of GCSE devices in the lateral direction.^{2,27,28} In fact, we have recently demonstrated⁴⁰ in-phase mode lasing of five resonant leaky-wave-coupled QCLs. Then, considering that typically ~67% of the coherent power is emitted in the array main far-field lobe, for a five-element phase-locked array of DFB/DBR QCLs coherent powers in excess of 10 W become possible.

In conclusion, a type of grating-surface-emitting laser is presented that offers efficient single-lobe lasing due to the antisymmetric modes being strongly absorbed via TM-mode resonant coupling to surface plasmon modes. By employing a published QCL-core structure, we find that DFB/DBR devices can lase in a single-lobe pattern with threshold currents as low as 0.45 A and slope efficiencies as high as 3.4 W/A. Thus, the devices hold potential for watt-range CW coherent-power emission delivered reliably, since emittingfacet heating and subsequent degradation are avoided.

This work was supported under Navy Contract No. N68335-11-C-0432 (K. K. Law).

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